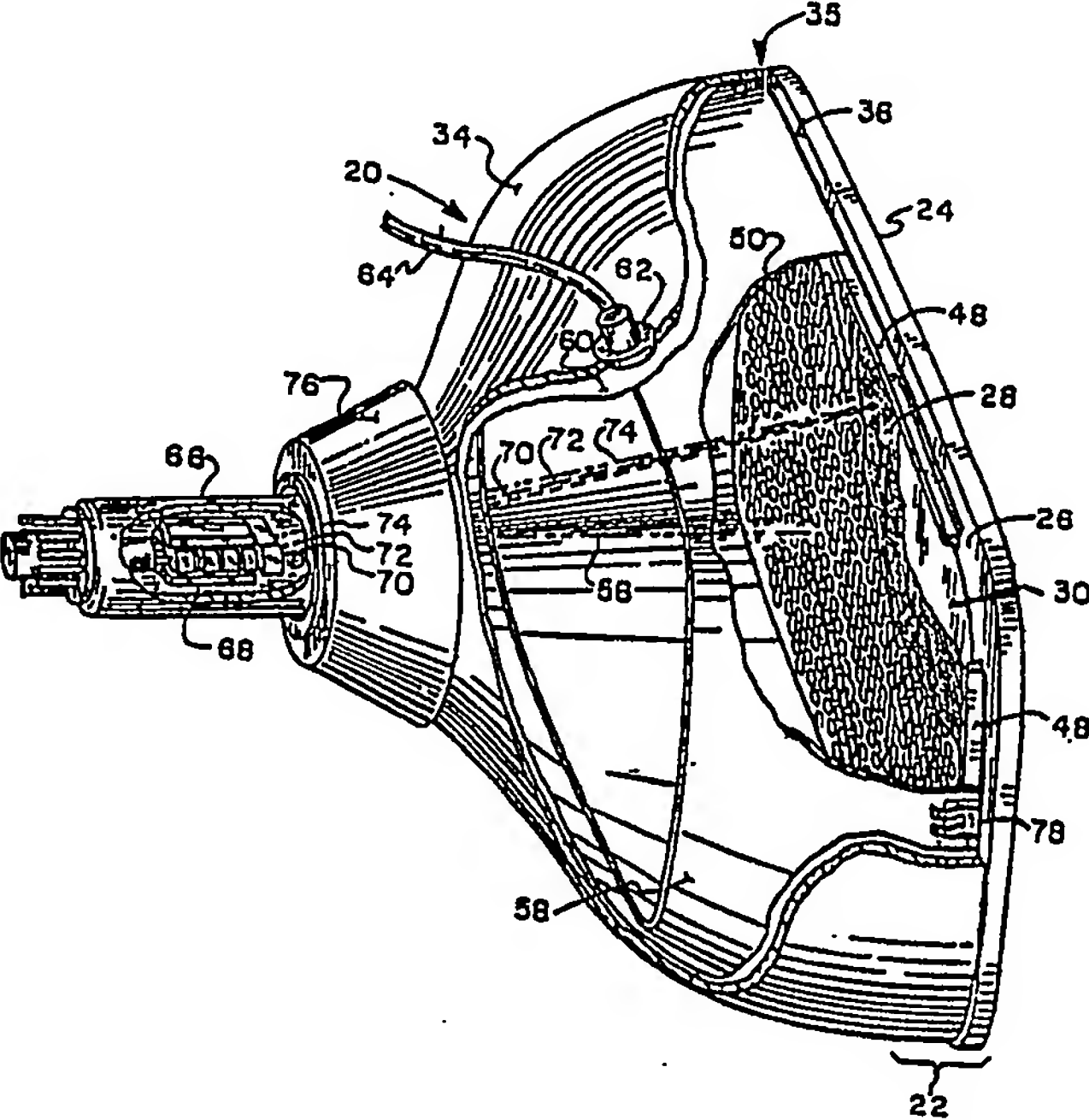




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(54) Title: BLACKENING OF NI-BASED FTM SHADOW MASKS  (57) Abstract <p>The power handling capacity of nickel-iron-based flat tensioned foil shadow masks for flat faceplate cathode ray tubes (CRTs) is enhanced by providing the flat tensioned mask (FTM) with a thin surface layer which is enriched in nickel, which is converted to a nickel phosphide compound. The nickel phosphide surface layer is formed on the mask by immersing the mask in a first bath of a strong reducing acid followed by immersing the mask in a second strong reducing acid having an effective amount of hypophosphite ion. The thin surface layer of a nickel phosphide compound increases the FTM emissivity and reduces FTM doming at high electron beam energies. The nickel phosphide compound may be stabilized in the frit-lehr cycle during CRT assembly or in a separate heating operation.</p>		

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BLACKENING OF NI-BASED FTM SHADOW MASKS

This invention relates generally to flat faceplate cathode ray tubes, and more particularly to tubes of this type which have a tensioned foil shadow mask made from an alloy comprising nickel and iron. The invention also relates to a process for the manufacture of such masks, including contacting the mask with a strong reducing acid which dissolves iron faster than nickel to provide a nickel rich surface layer followed by contacting the shadow mask with a mixture of a strong reducing acid and hypophosphite salt to provide improved shadow mask emissivity for accommodating high electron beam energies. Also disclosed is a cathode ray tube assembly containing such a mask.

Cathode ray tubes having flat faceplates and flat tensioned foil shadow masks are known to provide many advantages over conventional cathode ray tubes having a curved faceplate and a curved shadow mask. A chief advantage of a flat faceplate cathode ray tube with a tensioned mask is a greater electron beam power-handling capability, a capability which can provide greater picture brightness. The power-handling capability of tubes having the conventional curved mask is limited due to the thickness of the mask (0.1m to 0.2m 5 to 7 mils), and the fact that it is not mounted under tension. As a result, the mask tends to expand or "dome" in picture areas of high brightness where the intensity of electron beam bombardment, and consequently the heat, is greatest. Color impurities result when the mask expands toward the faceplate and the beam-passing apertures in the mask move out of registration with their associated phosphor dots or lines on the faceplate.

A tensioned mask when heated acts in a manner quite different from a curved, untensioned mask. For example, if the entire mask is heated uniformly, the mask expands and relaxes the tension. The mask remains planar and there is no doming and no distortion until the mask

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has expanded to the point that tension is completely lost. Just before all tension is lost, wrinkling may occur in the corners. When small areas of a tensioned foil mask are differentially heated, the heated areas expand and the unheated areas correspondingly contract, resulting in only small displacements within the plane of the mask. However, the mask remains planar and properly spaced from the faceplate and, consequently, any color impurities are unnoticeable.

The mask must be supported in tension in order to maintain the mask in a planar state during operation of the cathode ray tube. The amount of tension required will depend upon how much the mask material expands upon heating during operation of the cathode ray tube. Materials with very low thermal coefficients of expansion need only a low tension. Generally, however, the tension should be as high as possible because the higher the tension, the greater the heat incurred, and the greater the electron beam current that can be handled. There is a limit to mask tension, however, as too great a tension can cause the mask to tear.

The mask may be tensioned in accordance with known practices. A convenient method is to thermally expand the mask by means of heated platens applied to both sides of the mask. The expanded mask is then clamped in a fixture and, upon cooling, remains under tension. The mask may also be expanded by exposure to infrared radiation, by electrical resistance heating, or by stretching through the application of mechanical forces to its edges.

Prior Art

It is well known in the manufacture of standard color cathode ray tubes of the curved-mask, curved-screen type to heat-treat the masks prior to their being formed

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into a domed shape. Conventional (non-tensioned) masks are typically delivered to cathode ray tube manufacturers in a work-hardened state due to the multiple rolling operations which are performed on the steel to reduce it to the specified thickness, typically about 6 mils. In order that the masks may be stamped into a domed shape, they must be softened by use of an annealing heat treatment--typically to temperatures on the order of 700-800°C. Annealing also enhances the magnetic coercivity of the masks, a desirable property from the standpoint of magnetic shielding of the electron beams. After stamping, and the consequent moderate work hardening of the mask which may result from the stamping operation, it is known in the prior art to again anneal the masks while in their domed shape to further enhance their magnetic shielding properties.

Foils intended for use as tensioned masks are also delivered in a hardened state--in fact, much harder than standard masks in order to provide the very high tensile strength needed to sustain the necessary high tension levels; for example, 2109 kg/cm² (30,000 psi), or greater. The prior art annealing process, with its relatively high annealing temperatures, would be absolutely unacceptable if applied to flat tension masks, as any extensive softening or reduction of tensile strength of the mask resulting from the process would make the material unsuited for use as a tension mask.

U.S. Patent No. 4,210,843 sets forth an improved method of making a conventional color cathode ray tube shadow mask; that is, a curved shadow mask having a thickness of about 6 mils, and designed for use with a correlatively curved faceplate. The method comprises providing a plurality of mask blanks composed of an interstitial-free steel, each with a pattern of apertures photo-etched therein, which blanks have been cut from a foil of steel, precision cold-rolled to a full hard

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condition, and with a thickness of from 6 to 8 mils. A stack of blanks is subjected to a limited annealing operation carried out at a relatively low maximum temperature, and for a relatively brief period sufficient only to achieve recrystallization of the material without causing significant grain growth. Each blank is clamped and drawn to form a dished mask without the imposition of vibrating or roller leveling operations, and thus avoids undesired creasing, roller marking, denting, tearing or work-hardening of the blank normally associated with these operations. The end-product mask, due to the use of the interstitial-free steel material, has an aperture pattern of improved definition as a result of more uniform stretching of the mask blank. The annealing operation has little effect on the magnetic properties of this type of steel, and the coercivity of the material, after forming, is about 2.0 oersteds.

A foil shadow mask is maintained under high tension within the cathode ray tube, and the mask is subjected to predetermined relatively high temperatures during tube manufacture.

Earlier foil mask materials have limitations in terms of the desired combination of mechanical and magnetic properties described herein. One material used for mask applications in flat faceplate cathode ray tubes has been aluminum-killed (AK), AISI 1005 cold-rolled capped steel, generally referred to as "AK steel." AK steel has a composition of 0.04 percent silicon, 0.16 percent manganese, 0.028 percent carbon, 0.020 percent phosphorus, 0.018 percent sulfur, and 0.04 percent aluminum, with the balance iron and incidental impurities. Throughout the specification and claims, all percentages and parts are considered weight-percentages and parts by weight, unless otherwise indicated. Invar, which has a nominal composition of 36 percent nickel, balance iron, has also been suggested as a possible

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material for tensioned foil shadow masks. Invar however has a thermal coefficient of expansion far lower than that of the glass commonly used in cathode ray tube faceplates and so is considered generally unacceptable.

AK steel, while it can be formed into a fairly acceptable foil shadow mask, is deficient in certain important properties. For example, the yield strength of AK Steel foil one mil thick is typically in the range of 75-80 ksi. This makes it only marginally acceptable from a strength standpoint. More importantly, AK steel has a permeability that is much lower than desired, for example, 5,000 in a foil of 0.02m thickness (1 mil). Since the ability of a material to carry magnetic flux decreases with decreasing cross section, cathode ray tubes having masks made of AK steel thinner than about 1 mil may require both internal and external magnetic shielding. With internal shielding only, the beam landing misregistration due to the earth's magnetic field, i.e., the change in beam landing position upon reversal of the axial field component, is typically .025m (1.5 mils), which is much greater than the maximum of about .02m (1 mil) that is generally considered tolerable.

In addition, AK steel is metallurgically dirty, having inclusions, defects and dislocations which interfere with both the foil rolling process and the photo resist etching of the apertures in the foil resulting in higher scrap rates and consequently lower yields.

Another significant disadvantage of an AK steel tensioned foil shadow mask is the fact that as the tension applied is increased, the permeability decreases and the coercivity increases. Translated into picture performance, this means that as the tension of the AK foil shadow mask is increased in order to permit increased beam current and, therefore, greater picture brightness, its ability to shield the electron beams from the earth's magnetic field deteriorates, resulting in increased beam misregistration.

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U.S. Patent No. 3,867,207 describes a method for blackening steel components of a cathode ray tube, such as the aperture mask, by immersing the component in an electroless nickel or cobalt plating bath to provide a surface layer of nickel or cobalt on the component and, after subsequent rinses, immersing the component in a strong oxidizing acid and firing the component in air at about 450°C. to form a black, complex nickel or cobalt phosphide compound on the surface of the component.

The present invention overcomes the aforementioned limitations of the prior art by providing a shadow mask for use in a color cathode ray tube having a flat faceplate, said shadow mask characterized by a nickel-iron-based apertured foil; a thin surface layer of a nickel phosphide compound to increase its emissivity, said nickel of said surface layer of nickel phosphide being provided from the nickel of an iron-depleted surface region of said foil.

Preferably, the thin surface layer comprises a blackened nickel compound which substantially increases the emissivity of the shadow mask and retards its rate of temperature increase, thus reducing color purity loss (shadow mask doming) at high electron beam energies and which is provided by a simple process.

Objects of the Invention

Another feature of the present invention is to provide an improved process for fabricating a cathode ray tube incorporating a flat tensioned foil shadow mask.

A further feature of the present invention is to provide a flat tensioned foil shadow mask having improved mechanical and emissivity properties.

Yet another feature of the present invention is to provide for the treatment of prior art flat tensioned foil shadow masks so as to substantially increase their

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thermal radiation characteristics and current handling capabilities.

Brief Description of the Drawings

The features of the present invention which are believed to be novel are set forth with particularity in the appended claims. The invention, together with further objects and advantages thereof, may best be understood by reference to the following description taken in conjunction with the accompanying drawings (not to scale), wherein like reference numerals identify like elements, and in which:

Figure 1 is a side view in perspective of a color cathode ray tube having a flat faceplate and a tensioned foil shadow mask, with cut-away sections that indicate the location and relation of the faceplate and tensioned foil shadow mask to other major tube components;

Figure 2 is a plan view of an in-process foil shadow mask;

Figure 3 is a plan view of an in-process flat glass faceplate showing a phosphor screening area and a foil shadow mask support structure secured thereto;

Figure 4 is a perspective view of a funnel referencing and fritting fixture, with a funnel and the faceplate to which it is to be attached shown as being mounted on the fixture;

Figure 5 is a partial detail view in section and in elevation depicting the attachment of a funnel to a faceplate;

Figure 6 is a flow chart illustrating in simplified form the steps carried out in producing a tensioned foil shadow mask in accordance with the present invention;

Description of the Preferred Embodiment

To facilitate understanding of the process and material according to the invention and their relation to the manufacture of a color cathode ray tube having a tensioned foil shadow mask, a brief description of a tube of this type and its major components is offered in the following paragraphs.

A color cathode ray tube 20 having a tensioned foil shadow mask is depicted in FIG. 1. The faceplate assembly 22 essentially comprises a flat faceplate and a tensioned flat foil shadow mask mounted adjacent thereto. Faceplate 24, indicated as being rectangular, is shown as having on its inner surface 26 a centrally located phosphor screen 28 depicted diagrammatically as having a pattern of phosphors thereon. A film of aluminum 30 is indicated as covering the pattern of phosphors. A funnel 34 is represented as being attached to faceplate assembly 22 at their interfaces 35; the funnel sealing surface 36 of faceplate 24 is indicated as being peripheral to screen 28. A frame-like shadow mask support structure 48 is indicated as being located on opposed sides of the screen between funnel sealing surface 36 and screen 28, and mounted adjacent to faceplate 24. Support structure 48 provides a surface for receiving and mounting in tension a metal foil shadow mask 50 a Q-distance away from the screen 28. The pattern of phosphors corresponds to the pattern of apertures in mask 50. The apertures depicted are greatly exaggerated for purposes of illustration; in a high-resolution color tube for example, the mask has as many as 750,000 such apertures, with aperture diameter being on the average about 0.01cm (5 mils). As is well-known in the art, the foil shadow mask acts as a color-selection electrode, or "parallax barrier" which ensures that each of the beamlets formed by the three beams lands only on its assigned phosphor deposits on the screen.

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The anterior-posterior axis of tube 20 is indicated by reference number 56. A magnetic shield 58 is shown as being enclosed within funnel 34. High voltage for tube operation is indicated as being applied to a conductive coating 60 on the inner surface of funnel 34 by way of an anode button 62 connected in turn to a high-voltage conductor 64.

The neck 66 of tube 20 is represented as enclosing an in-line electron gun 68 depicted as providing three discrete in-line electron beams 70, 72 and 74 for exciting respective red-light-emitting, green-light-emitting, and blue-light-emitting phosphor elements deposited on screen 28. Yoke 76 receives scanning signals and provides for the scanning of beams 70, 72 and 74 across screen 28. An electrical conductor 78 is located in an opening in shield 58 and is in contact with conductive coating 60 to provide a high-voltage connection between the coating 60, the screen 28, and shadow mask 50.

Two of the major components, designated as being "in-process," are depicted and described as follows. One is a shadow mask indicated diagrammatically in FIG. 2. In-process shadow mask 86 includes a central area 104 of apertures corresponding to the pattern of phosphors that is photodeposited on the screen of the faceplate by using the mask as an optical stencil. Center field 104 is indicated as being surrounded by an unperforated section 106, the periphery of which is engaged by a tensing frame during the mask tensing and clamping process, and which is removed in a later procedure.

An in-process faceplate 108 is depicted diagrammatically in FIG. 3 as having on its inner surface 110 a centrally located screening area 112 for receiving a predetermined phosphor pattern in an ensuing operation. A funnel sealing surface 113 as indicated as being peripheral to screen 112. A frame-like shadow mask

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support structure 114 is depicted as being secured on opposed sides of screen 112; the structure provides a surface 115 for receiving and mounting a foil shadow mask under tension a Q-distance from the screen.

A process according to the invention preferably comprises providing an apertured foil shadow mask 86 comprised of a nickel-iron alloy, and securing the mask 86 to the mask support structure 114 of the faceplate 108 while under tension, and in registration with the phosphor screen. The process is further characterized by first subjecting the mask 86 to contact with a strong reducing acid which dissolves iron faster than nickel to provide a nickel-rich surface layer followed by blackening the surface layer by contacting the mask with a mixture of a strong reducing acid and a hypophosphite salt to provide a blackened surface layer of nickel and molybdenum phosphides.

A class of nickel-iron alloys, desirably containing minor additions of certain alloying agents, when heat-treated and cooled under controlled conditions, yield a material which, when fabricated into a thin foil, has mechanical and magnetic properties not found in known alloys that makes them uniquely suited for use as tensioned foil shadow masks.

With regard to the alloy composition, a nickel-iron alloy is provided comprising between about 30 and 85 weight-percent of nickel, between about 0 and 5 weight-percent of molybdenum, between 0 and 2 weight-percent of one or more of vanadium, titanium, hafnium, and niobium, with the balance iron and incidental impurities; e.g., carbon, chromium, silicon, sulfur, copper and manganese. Typically, the incidental impurities combined do not exceed 1.0 percent. Preferably the alloy may comprise between about 75 and 85 weight-percent of nickel, between about 3 and 5 weight-percent of molybdenum, with the balance iron and

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incidental impurities. Most preferably, the alloy may comprise about 80 weight-percent nickel, about 4 weight-percent molybdenum, with the balance iron and incidental impurities. These examples of foil mask materials are generally referred to as molypermalloys.

Mask Heat Treatment During Frit Cycle

The heat treatment of the masks described in the following paragraphs closely approximates the processing steps in frit sealing cathode ray tube, and the sealing of the funnel and faceplate in the manufacturing process.

As indicated in FIG. 3 a shadow mask support structure 114 is secured on the inner surface 110 of faceplate 108 between the peripheral sealing area, noted as being the funnel sealing surface 113, and the screening area 112. The mask support structure 114 provides a surface 115 for receiving and supporting a foil shadow mask in tension. The mask support structure 114 may comprise, by way of example, a stainless steel metal alloy or alternately, a ceramic structure. Attachment of the support structure is preferably by means of a devitrifying frit.

The alloy according to the invention is formed into a foil having a thickness of about 0.02m (0.001 inch) or less. A central area 112 of the foil is apertured to form a foil mask 108 consonant in dimensions with the screening area 112 for color selection. Aperturing of the mask can be accomplished by a photo-etching process in which a light-sensitive resist is applied to the foil. The resist is hardened by exposure to light except in those areas where apertures are defined. The exposed metal defining the apertures is then etched away.

The foil mask is then tensed in a tensing frame to a tension of at least about 25 Newton/centimeters. In essence, the foil may be expanded by enclosing it between

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two platens heated to 360°C. for one minute, clamped in the tensing frame, and air cooling it to provide a tensioned foil having a greater length and width than the faceplate to which it will be secured. A pattern of red-light-emitting, green-light-emitting, and blue-light-emitting phosphor deposits are sequentially photoscreened on screening area 112. The photoscreening process includes repetitively registering the foil to the phosphor screening area by registering the tensing frame with the faceplate in a well known manner.

The foil comprising the mask 86 is secured to the mask support structure 114, with the apertures of the mask in registration with the pattern of phosphor deposits on screening area 112. The means for securing the mask to the mask support structure may be by welding with a laser beam, with the excess mask material being removed by the same beam. Inasmuch as the faceplate 108 and tensioned foil shadow mask 86 are rigidly interconnected by their mutual attachment to the mask support structure, the thermal coefficient of expansion of the alloy foil must approximate that of the faceplate, which is typically a glass having a coefficient of expansion of between about 12×10^{-6} in/in/°C. This is necessary due to the relatively high temperatures to which the faceplate and mask are subjected during the cathode ray tube manufacturing process. A coefficient of expansion somewhat greater than that of the faceplate can be tolerated, but a coefficient of expansion substantially less than that of the faceplate is to be avoided as this may lead to mask failure during the manufacturing process.

FIGS. 4 and 5 depict the use of a funnel referencing and fritting fixture 186 for mating of a faceplate 108 with a funnel 188 to form a faceplate-funnel assembly. Faceplate 108 is indicated as being installed face down on the surface 190 of fixture 186. Funnel 188 is depicted as being positioned thereon and in contact

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with funnel sealing surface 113, noted as being peripheral to screening area 112 on which is deposited a pattern of phosphors 187 as a result of the preceding screening operation. With reference to FIG. 4, three posts 192, 193 and 194 are indicated as providing for alignment of the funnel and faceplate. FIG. 5 depicts details of the interface between post 194, the faceplate 108, and funnel 188. Flat 117c on faceplate 108 is shown as being in alignment with reference area "c" on funnel 188. Shadow mask 86, noted as being in tension, is depicted as being mounted on shadow mask support structure 114; this configuration of a shadow mask support structure is the subject of U.S. Patent No. 4,686,416.

Post 194 is shown as having two reference points 196 and 198 for locating the funnel 188 with reference to the faceplate 108. The reference points preferably comprise buttons of carbon as they must be immune to the effects of the elevated oven temperature incurred during the frit cycle.

A devitrifiable frit in paste form is applied to the peripheral sealing area of the faceplate 108, noted as being funnel sealing area 113, for receiving funnel 188. The faceplate 108 is then mated with the funnel 188 to form a faceplate-funnel assembly. The frit, which is indicated by reference No. 200 in FIG. 5, may for example, comprise frit No. CV-130, manufactured by Owens-Illinois, Inc. of Toledo, Ohio.

The faceplate-funnel assembly is then heated to a temperature effective to devitrify the frit and permanently attach the funnel to the faceplate, after which the assembly is cooled. The process of fusing of the funnel to the faceplate is generally carried out under conditions referred to as the frit cycle. In a typical frit cycle, the faceplate, to which the tensioned foil mask is adhered, and funnel are slowly heated to 435°C., then cooled to room temperature or slightly thereabove

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over a period of 3 - 3-1/2 hours. The foil must be cooled to the temperature at which the alloy is substantially recrystallized at a cooling rate of less than about 5°C. per minute, preferably less than about 3°C. per minute, and most desirably at a rate of between about 2°C. and about 3°C. per minute. The heating of the assembly and the foil is effective to blacken, or oxidize, a thin surface layer of a nickel compound deposited on the foil mask in accordance with the present invention as described in detail below.

Referring to FIG. 6, there is shown a simplified flow chart for a procedure for treating a foil mask in accordance with the principles of the present invention. The first step at block 210 in the process involves degreasing of the foil tension mask (FTM). The FTM may be degreased by dipping it into a hot alkaline solution for on the order of 10 minutes. The next step at block 212 is the ultrasonic cleaning of the degreased FTM. The degreasing and ultrasonic cleaning procedures remove contaminants from the surface of the FTM which decrease the effectiveness of the subsequent steps.

At step 214, the FTM is immersed in a strong reducing acid bath. Since iron has an electrochemical potential of -440mV as compared to the electrochemical potential of -250mV for nickel, the iron can be selectively removed from the surface of the FTM to provide a nickel enriched surface layer. The preferred strong reducing acid is preferably concentrated hydrochloric acid having from about 38% to about 50% HCL. The FTM preferably remains in contact with the strong reducing acid for a period of from about 1 to about 10 minutes while the acid is maintained at a temperature of from about 25 to about 75°C. After treatment with the strong reducing acid a nickel enriched surface layer from about .025cm (.01) to about .25cm (.1 mil) thick is formed which has an average nickel content of from about 75% to about

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96% with the balance being primarily molybdenum. After being treated with a strong reducing acid, the FTM is cleaned with water at step 216.

At step 218, the FTM is immersed into a strong reducing acid having a substantial level of hypophosphite ions. A suitable reducing acid is concentrated hydrochloric acid having from about 38% to about 50% HCL. The reducing acid is mixed with an effective amount of a soluble hypophosphite salt, such as sodium hypophosphite or potassium hypophosphite. Any hypophosphite salt which has a solubility of at least about 75 grams in 25°C. water can be used. Preferably, the hypophosphite salt is added to the strong reducing acid at a level from about 50 grams to about 250 grams per liter. The FTM preferably remains in contact with the mixture of acid and hypophosphite salt for a period of from about 5 to about 30 minutes while the acid is maintained at a temperature of from about 25 to about 85°C. After treatment with the mixture of acid and hypophosphite salt, the nickel in the nickel enriched layer (and any molybdenum which may be present) are converted to complex nickel or molybdenum phosphide compounds, such as Ni_3P_2 , which are black in color. After acid treatment, the FTM is then cleaned in tap water at step 220 to remove any excess acid solution, followed by air blow drying of the iron coated FTM at step 222. The FTM may then be stored until required for use as a shadow mask in the manufacture of flat faceplate cathode ray tubes.

It should be understood that discrete steps 214 and 218 are not required. That is, the formation of the nickel enriched surface layer, as depicted in Step 214, and the conversion of the nickel (and any molybdenum which may be present) to complex phosphide compounds, as depicted in step 218, can be accomplished in a single step by immersing the FTM into a strong reducing acid having a substantial level of hypophosphite ions. This alternate

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method for forming the blackened surface layer of nickel and molybdenum phosphide compounds is shown by the dashed line route in FIG. 6.

After treatment in accordance with the invention to provide a blackened surface layer of complex nickel phosphide compounds, the complex nickel phosphide compound surface layer of the FTM may be stabilized at step 224 by heat treatment prior to use or such stabilization may take place during the first cycle used in the manufacture of the cathode ray tube. In this connection, the complex nickel phosphide compound formed on the surface of the FTM is easily abraded and care must be exercised in handling the FTM prior to the stabilization heat treatment.

In one example of the present invention, the foil mask is heated to a temperature of 435°C. for 55 minutes to effect stabilization. The stabilized and blackened Ni_3P_2 surface layer substantially increases the heat dissipating capability of the foil mask and retards the rate of temperature increase of the mask upon bombardment by electron beams by efficiently and effectively radiating away heat buildup so as to minimize its thermal distortion. Heating of the foil mask may be accomplished either before or after the foil mask is secured to the faceplate of a cathode ray tube. In the latter case, foil mask heating may be accomplished during a conventional frit-lehr cycle as described above. In heating the foil mask during the frit-lehr cycle, the assembled faceplate and funnel together with the foil mask was positioned on a belt moving at a speed of 9 inches per minute and was passed through an open furnace and exposed to a peak temperature of 435°C. for 55 minutes. Subjecting the foil mask to temperatures in the range 400°C. to 600°C. for a period ranging from 1/2 hour to 1 hour has also resulted in stabilizing of the foil mask and a substantial increase in its emissivity.

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Referring to Table I, there is shown the results of emissivity measurements of foil masks. The emittance data was taken at 40°C. using a typical IR spectrometer. The upper row of data is for a foil mask treated in accordance with the invention to provide a surface layer of Ni_3P_2 . Measurements were made in the infrared spectrum at various wavelengths as indicated in the table.

TABLE I

Emissivity of Various Metal Masks
After Lehr Cycle

Material	Emissivity		
	5 M	8 M	14 M
Moly-Permalloy*			
Ni_3P_2 Surface Layer	0.878	0.782	0.306
AK Steel-Blackened	0.757	0.645	0.528

*Moly-Permalloy is the tradename for nickel alloy having 80% nickel, 4% molybdenum, 20% iron, balance impurities.

The lower row of data represents measured thermal emissivity for uncoated AK steel shadow masks after blackening by oxidizing heat treatment. From the measured data it can be seen that the emissivity of the molypermalloy masks treated in accordance with the invention closely approximates the thermal emissivity of prior art AK steel masks.

There has thus been shown in the preferred embodiment a nickel-iron-based flat tensioned foil shadow mask for use in a color cathode ray tube having a

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blackened, or oxidized, thin surface layer of a complex nickel phosphite compound which substantially increases the emissivity of the shadow mask and, by retarding its rate of temperature increase and reducing shadow mask doming, permits the shadow mask to operate at high electron beam energies and is economically and simply manufactured. More energetic electrons allow for increased brightness of the video image visible on the faceplate of the cathode ray tube. The thin surface layer of a complex nickel phosphite compound is formed on the flat tensioned foil shadow mask by subjecting the foil to successive baths of a strong reducing acid and a strong reducing acid having an effective level of hypophosphite in using a procedure readily adapted for large scale, commercial fabrication of cathode ray tubes with flat tensioned foil shadow masks. The thin surface layer of a complex nickel phosphite compound is then stabilized, either during frit sealing of the cathode ray tube or by subjecting the shadow mask to high temperature in a separate step.

While particular embodiments of the present invention have been shown and described, it will be obvious to those skilled in the art that changes and modifications may be made without departing from the invention in its broader aspects. Therefore, the aim in the appended claims is to cover all such changes and modifications as fall within the true spirit and scope of the invention. The matter set forth in the foregoing description and accompanying drawings is offered by way of illustration only and not as a limitation. The actual scope of the invention is intended to be defined in the following claims when viewed in their proper perspective based on the prior art.

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Claims

1. A shadow mask for use in a color cathode ray tube (20) having a flat faceplate (108), said shadow mask characterized by a nickel-iron-based apertured foil (50); a thin surface layer of a nickel phosphide compound to increase its emissivity, said nickel of said surface layer of nickel phosphide being provided from the nickel of an iron-depleted surface region of said foil (50).

2. The shadow mask of Claim 1 characterized in that said foil (50) is comprised of between about 75 and 85 weight-percent nickel, between about 3 and 5 weight-percent molybdenum, with the balance iron and incidental impurities.

3. The shadow mask of Claim 1 or 2 characterized in that said foil (50) is comprised of between about 30 and about 85 weight-percent nickel, between about 0 and 5 weight-percent molybdenum, between 0 and 2 weight-percent of one or more of vanadium, titanium, hafnium and niobium with the balance iron and incidental impurities.

4. The shadow mask of Claim 1 characterized in that said thin surface layer is from about .000025m to about .00025m (.01 mil - .1 mil) thick.

5. The shadow mask of Claim 1 or 4 characterized in that said thin surface layer is substantially nickel and molybdenum phosphides.

6. A shadow mask arrangement for use in a color cathode ray tube (20) having a flat faceplate (24), said shadow mask arrangement being characterized by a thin nickel-iron-based foil (50) having an apertured center portion and a solid peripheral portion, and tension means (48) for engaging the peripheral portion of said foil (50) and maintaining said foil (50) in a stretched condition, under tension, said foil (50) having a thin surface layer of a nickel phosphide compound to increase its emissivity, said nickel of said surface layer being provided from the nickel of an iron-depleted surface layer of said nickel-iron-based apertured foil.

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7. The shadow mask arrangement of Claim 6 characterized in that said thin surface layer is substantially nickel and molybdenum phosphide.

8. An improved nickel-iron-based foil shadow mask (50) for use in a color cathode ray tube (20) of the type having a plurality of apertures and which is maintained in a flat, stretched condition under tension, characterized in that said foil (50) has a thin surface layer of a nickel phosphide compound to increase its emissivity.

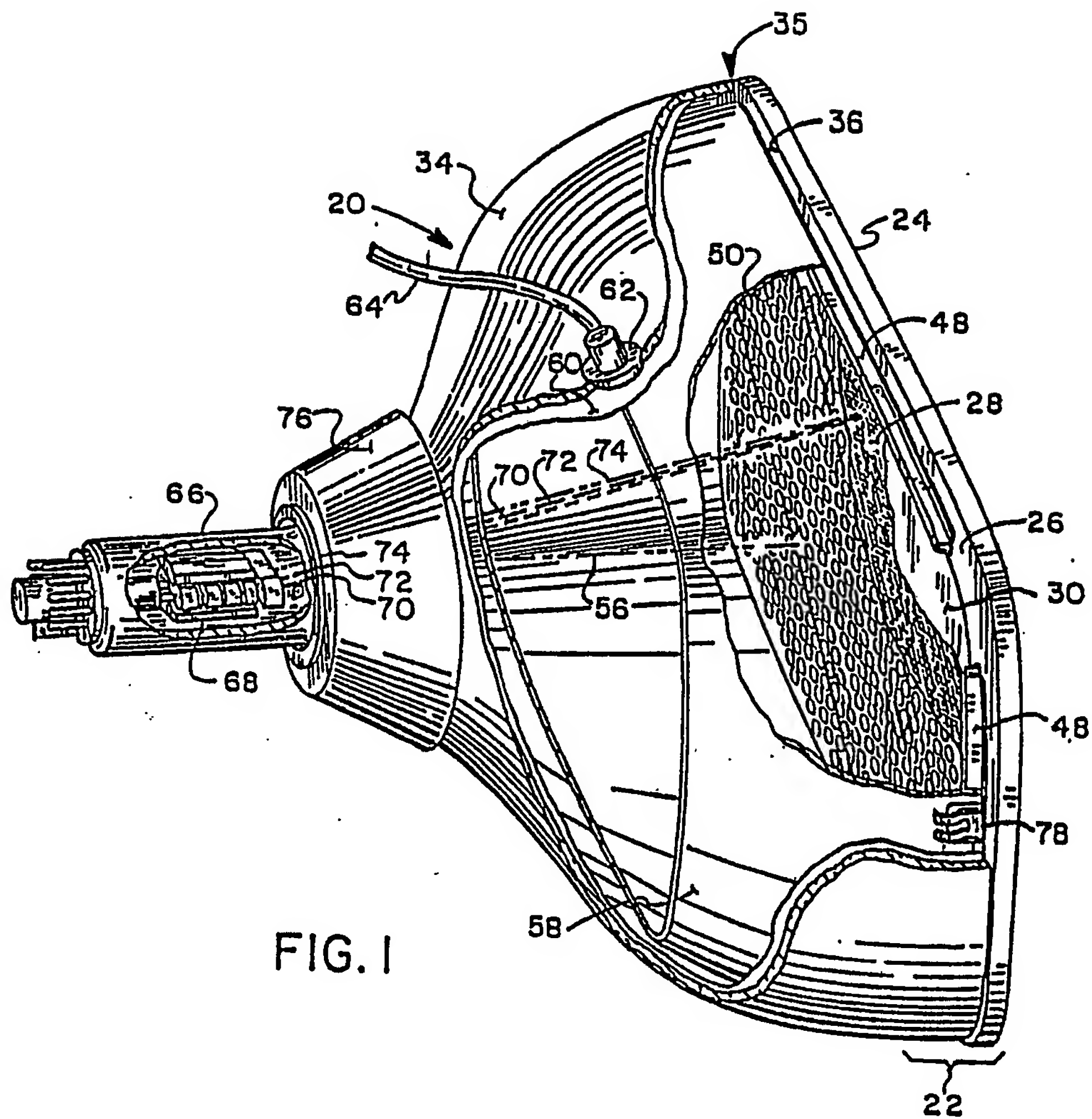


FIG. 1

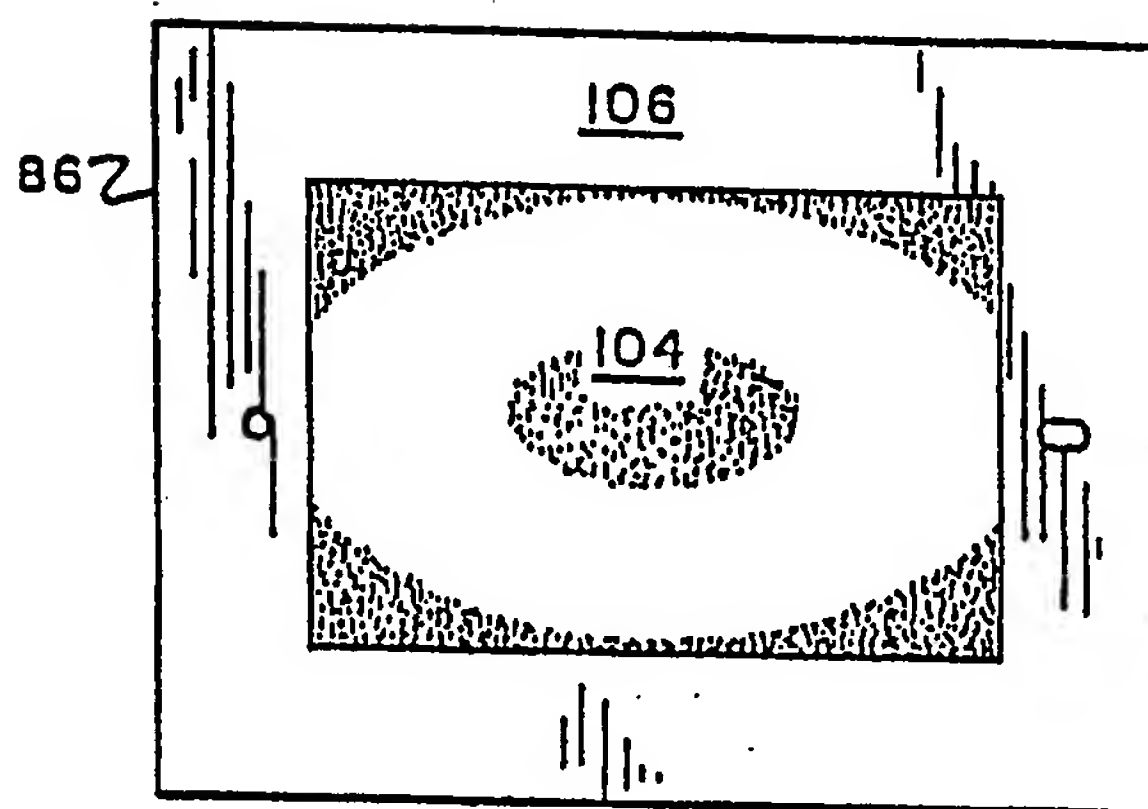


FIG. 2

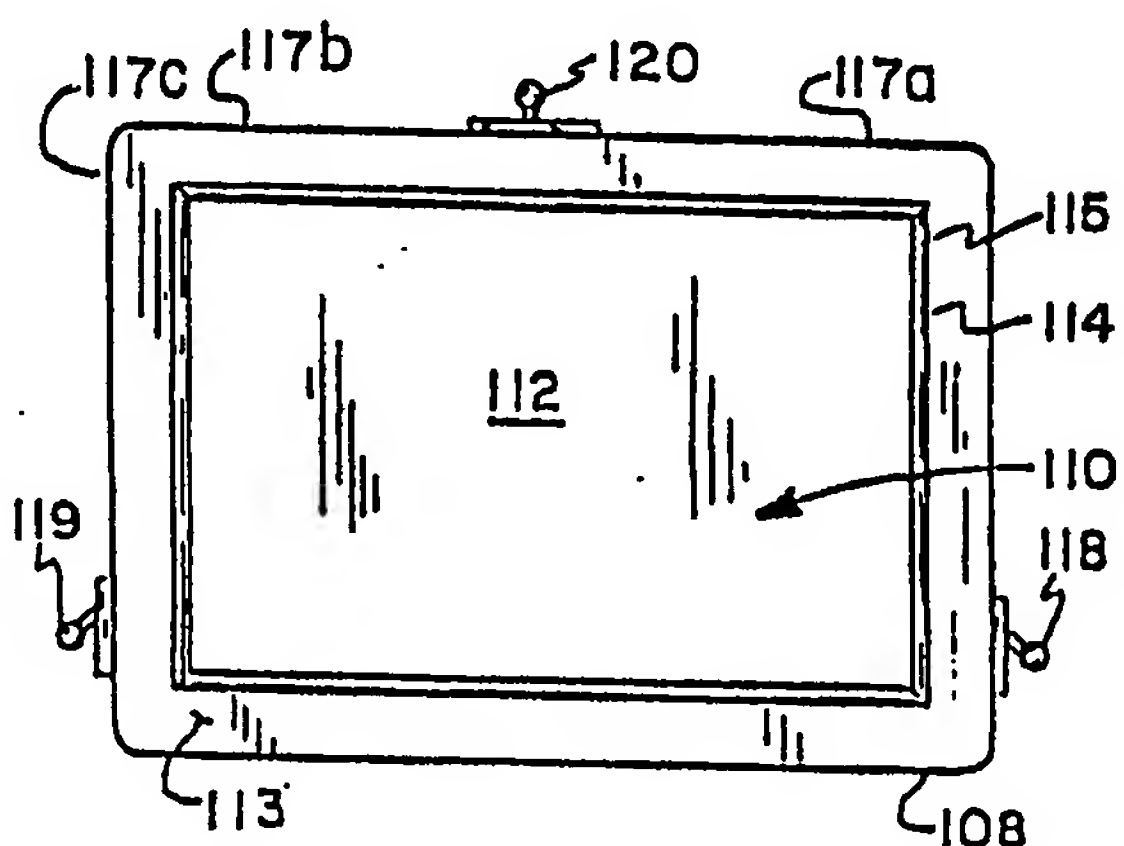


FIG. 3

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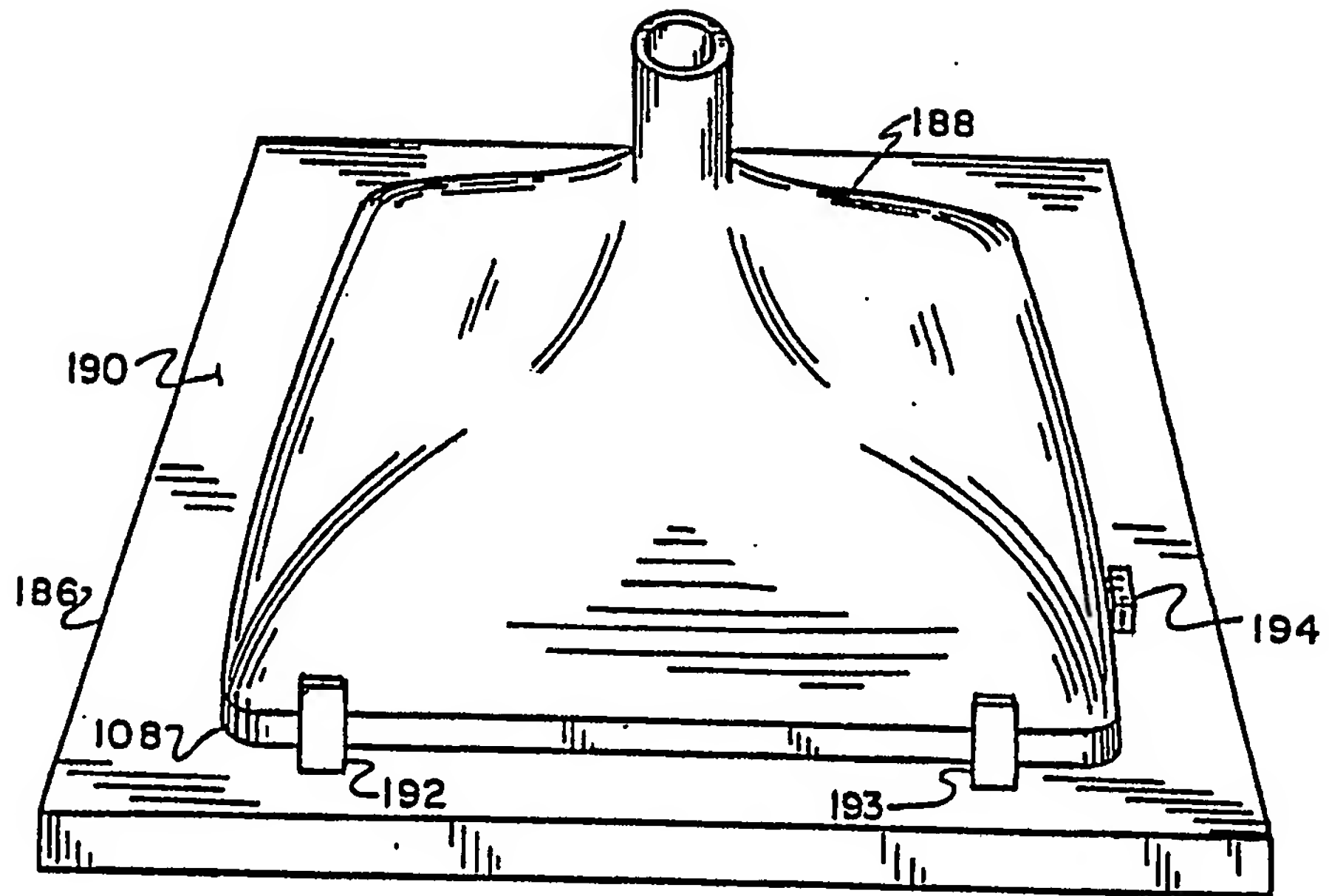


FIG. 4

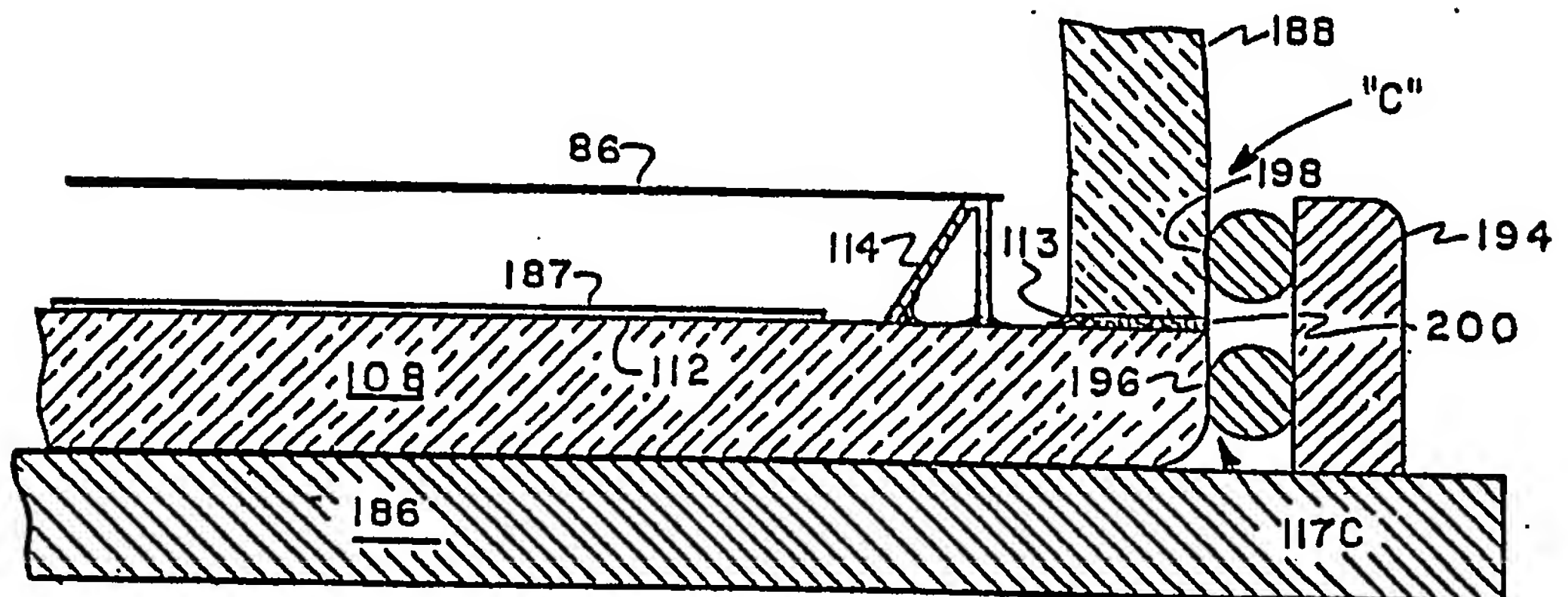
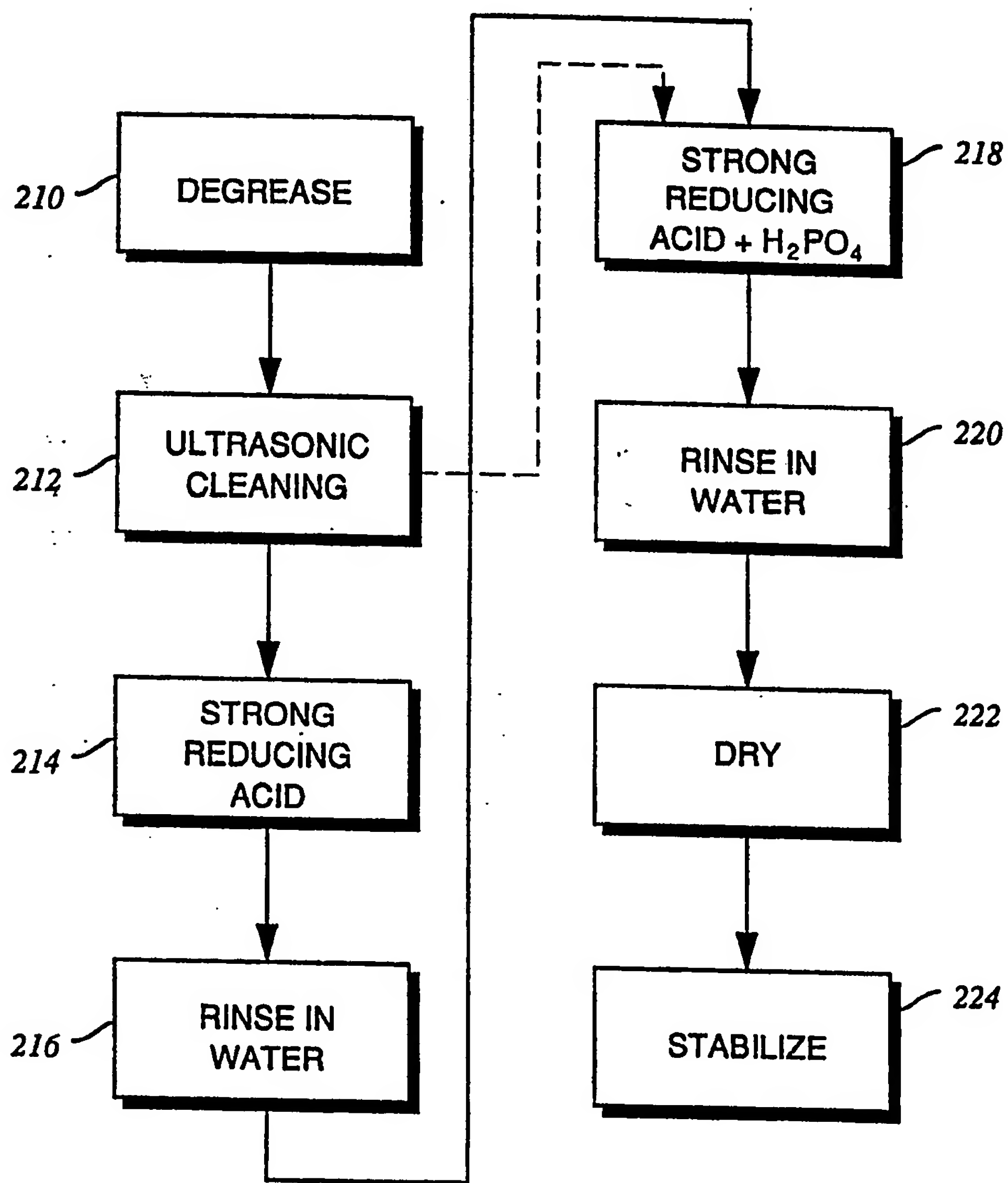


FIG. 5


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*Fig. 6*

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 90/01134

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) ⁶		
According to International Patent Classification (IPC) or to both National Classification and IPC		
Int.Cl. 5 H01J2907		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
Int.Cl. 5	H01J2900 ; H01J0900	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹		
Category ¹⁰	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
X	PATENT ABSTRACTS OF JAPAN vol. 12, no. 89 (E-592)(2936) 23 March 1988, & JP-A-62 223950 (TOSHIBA) 01 October 1987, see the whole document	1, 6, 8
Y		3
Y	PATENT ABSTRACTS OF JAPAN vol. 12, no. 186 (C-500)(3033) 31 May 1988, & JP-A-62 290846 (TOSHIBA) 17 December 1987, see the whole document	3
A	US,A,4767962 (ZENITH) 30 August 1988 see column 1, lines 23 - 32 see column 4, lines 40 - 47; figures 1, 3	1, 6, 8
<p>¹⁰ Special categories of cited documents :</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"I" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
28 JUNE 1990	16. 07. 90	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	ROWLES K.E.G. 	

PCT/US 90/01134
SA 35389

28/06/90

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A-4767962	30-08-88	None	